ECEN 615
Methods of Electric Power Systems Analysis

Lecture 24: EMP, Economic Dispatch, Optimal Power Flow

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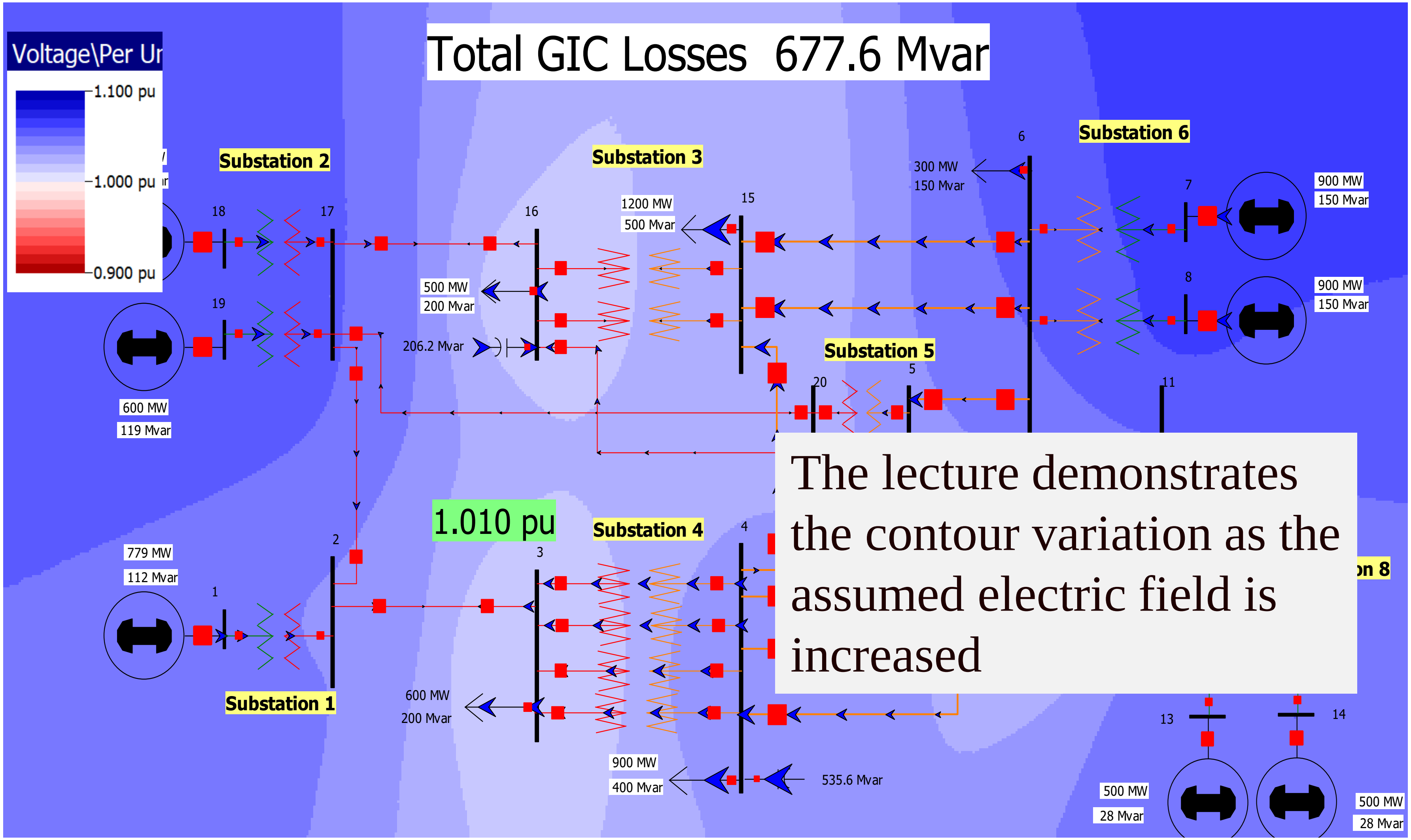
Announcements

- Homework 6 is due on Thursday Nov 27
- Read Chapters 3 and 8 (Economic Dispatch and Optimal Power Flow)
- Course evaluations are now available. Goto pica.tamu.edu
  - Please do the evaluation!!

20 Bus GIC Test System

- The dc parameters for a small GIC test system are defined in
  - R. Horton, D. Boteler, T.J. Overbye, R. Pirjola, R.C. Dugan, "A Test Case for the Calculation of Geomagnetically Induced Currents," IEEE Transactions on Power Delivery, vol. 27, pp. 2368-2373, October 2012
  - This paper did not define the ac power flow parameters
- Slides from last time showed the voltage contour values as the assumed electric field was increased

GIC_20BusTestCase



The lecture demonstrates the contour variation as the assumed electric field is increased

The Impact of a Large GMD From an Operations Perspective

- Maybe a day warning but without specifics
  - Satellite at Lagrange point one million miles from earth would give more details, but with less than 30 minutes lead time
  - Could strike quickly; rise time of minutes, rapidly covering a good chunk of the continent

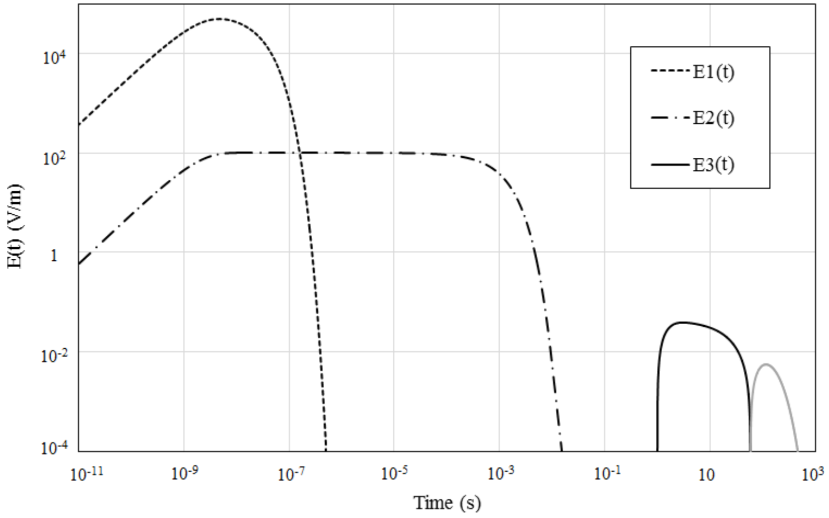
- Reactive power loadings on hundreds of high voltage transformers could rapidly rise

The Impact of a Large GMD From an Operations Perspective

- Increased transformer reactive loading causes heating issues and potential large-scale voltage collapses
- Power system software like state estimation could fail
- Control room personnel would be overwhelmed
- The storm could last for days with varying intensity
- Waiting until it occurs to prepare would not be a good idea!

Nuclear EMPs

- Broadly defined, an electromagnetic pulse (EMP) is any transient burst of electromagnetic energy
- High altitude nuclear explosions can produce continental scale EMPs; called HEMPs
- The impacts of an HEMP are typically divided into three time frames: E1, E2 and E3
  - E1 impacts electronics, E2 is similar to lightning, E3 is similar to a very large, but short duration GMD



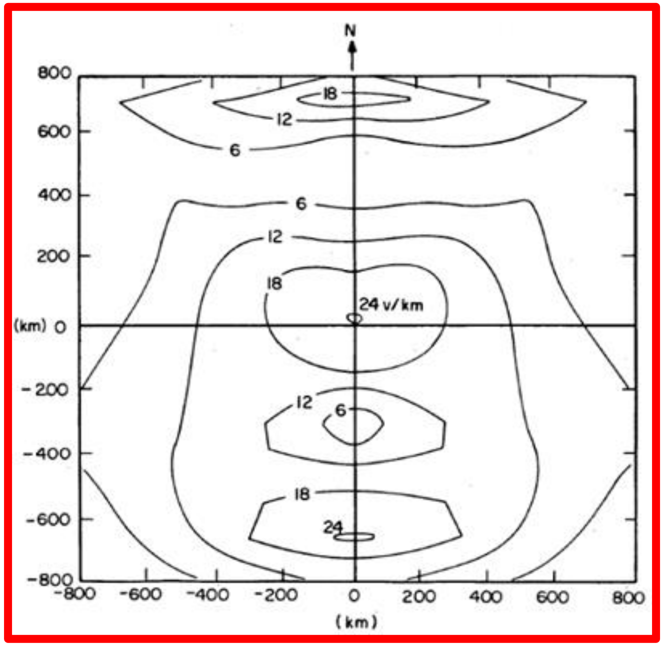
Nuclear EMP History: Starfish Prime

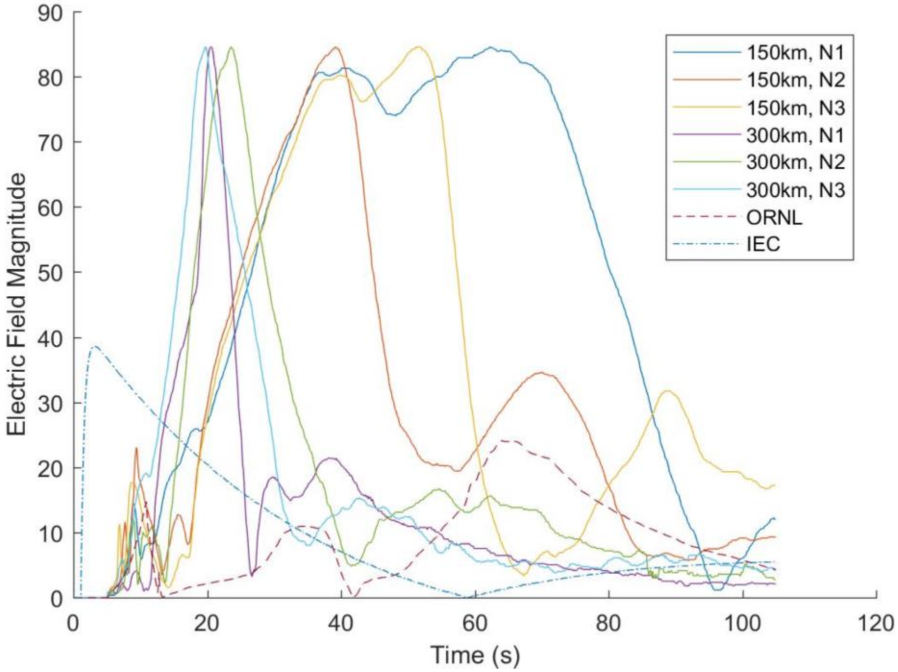
- HEMPs were theorized from the beginning; much of the public data is from tests in early 1960's
- Starfish Prime was an explosion of a 1.44 megaton nuclear weapon at an altitude of 400 km over the Pacific Ocean in July 1962
  - Part of series of tests known as Operation Fishbowl
  - The HEMPs were large, driving instruments off scale
  - Impacts seen in Honolulu (1445 km away), including knocking out about 300 street lights, setting off alarms, and damaging a microwave link; some satellites were also damaged

Starfish Prime flash seen in Honolulu; source: Wikipedia

HEMP Electric Field Waveforms

- 1985 – Oak Ridge National Labs (ORNL), 24 V/km
- 1996 – International Electrotechnical Commission (IEC)*, 40 V/km
- 2018 – EMP Commission, six waveforms, 84.57 V/km

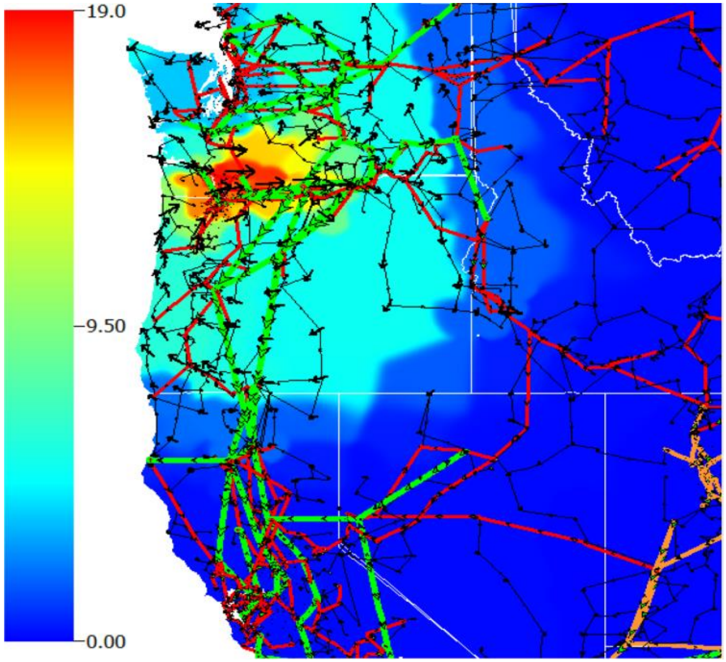




HEMP Including Ground Models

- See NAPS 2018 paper by R. Lee and T.J. Overbye, “Comparing the Impact of HEMP Electric Field Waveforms on a Synthetic Grid”

Image shows results for a 10,000 bus synthetic grid with an applied HEMP electric field centered at a latitude and longitude of 46.1°N, −121.6°W



Power System Economic Dispatch

- Generators can have vastly different incremental operational costs
  - Some are essentially free or low cost (wind, solar, hydro, nuclear)
  - Because of the large amount of natural gas generation, electricity prices are very dependent on natural gas prices
- Economic dispatch is concerned with determining the best dispatch for generators without changing their commitment
- Unit commitment focuses on optimization over several days. It is discussed in Chapter 4 of the book, but will not be not covered here

Power System Economic Dispatch

- Economic dispatch is formulated as a constrained minimization
  - The cost function is often total generation cost in an area
  - Single equality constraint is the real power balance equation
- Solved by setting up the Lagrangian (with P_D the load and P_L the losses, which are a function the generation)

$$\mathrm{L}(\mathbf{P}_{\mathrm{G}},\lambda) = \sum_{i=1}^{m} C_i(P_{Gi}) + \lambda\left(P_D + P_L(\mathbf{P}_G) - \sum_{i=1}^{m} P_{Gi}\right)$$

- A necessary condition for a minimum is that the gradient is zero. Without losses this occurs when all generators are dispatched at the same marginal cost (except when they hit a limit)

Power System Economic Dispatch

$$\mathrm{L}(\mathbf{P}_{\mathrm{G}},\lambda) = \sum_{i=1}^{m} C_i(P_{Gi}) + \lambda\left(P_D + P_L(P_G) - \sum_{i=1}^{m} P_{Gi}\right)$$

$$\frac{\partial \mathrm{L}(\mathbf{P}_{\mathrm{G}},\lambda)}{\partial P_{Gi}} = \frac{dC_i(P_{Gi})}{dP_{Gi}} - \lambda\left(1 - \frac{\partial P_L(P_G)}{\partial P_{Gi}}\right) = 0$$

$$P_D + P_L(P_G) - \sum_{i=1}^{m} P_{Gi} = 0$$

- If losses are neglected then there is a single marginal cost (lambda); if losses are included then each bus could have a different marginal cost

Economic Dispatch Penalty Factors

Solving each equation for λ we get

$$\frac{dC_i(P_{Gi})}{dP_{Gi}} - \lambda(1 - \frac{\partial P_L(P_G)}{\partial P_{Gi}} = 0$$

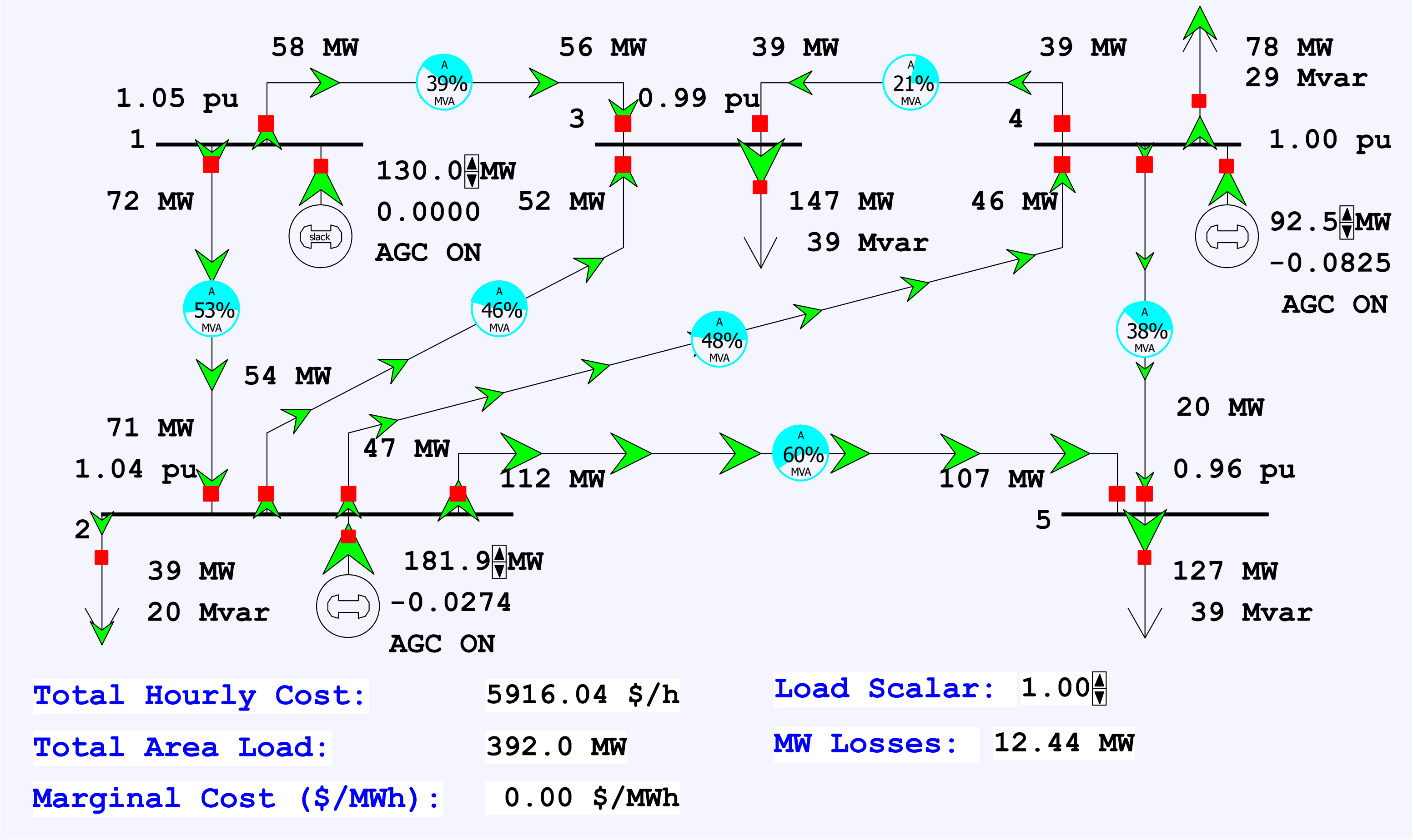
$$\lambda = \frac{1}{\left(1 - \frac{\partial P_L(P_G)}{\partial P_{Gi}}\right)} \frac{dC_i(P_{Gi})}{dP_{Gi}}$$

Define the penalty factor L_i for the i^{th} generator

$$L_i = \frac{1}{\left(1 - \frac{\partial P_L(P_G)}{\partial P_{Gi}}\right)}$$

The penalty factor at the slack bus is always unity!

Economic Dispatch Example



Total Hourly Cost: 5916.04 $/h

Total Area Load: 392.0 MW

Marginal Cost ($/MWh): 0.00 $/MWh

Load Scalar: 1.00

MW Losses: 12.44 MW

Case is GOS_Example6_22; use **Power Flow Solution Options, Advanced Options** to set Penalty Factors

Optimal Power Flow (OPF)

- OPF functionally combines the power flow with economic dispatch
- SCOPF adds in contingency analysis
- Goal of OPF and SCOPF is to minimize a cost function, such as operating cost, taking into account realistic equality and inequality constraints
- Equality constraints
  - bus real and reactive power balance
  - generator voltage setpoints
  - area MW interchange

OPF, cont.

- Inequality constraints
  - transmission line/transformer/interface flow limits
  - generator MW limits
  - generator reactive power capability curves
  - bus voltage magnitudes (not yet implemented in Simulator OPF)
- Available Controls
  - generator MW outputs
  - transformer taps and phase angles
  - reactive power controls

Two Example OPF Solution Methods

- Non-linear approach using Newton’s method
  - handles marginal losses well, but is relatively slow and has problems determining binding constraints
  - Generation costs (and other costs) represented by quadratic or cubic functions
- Linear Programming
  - fast and efficient in determining binding constraints, but can have difficulty with marginal losses.
  - used in PowerWorld Simulator
  - generation costs (and other costs) represented by piecewise linear functions
- Both can be implemented using an ac or dc power flow

OPF and SCOPF Current Status

- OPF (really SCOPF) is currently an area of active research, with ARPA-E having an SCOPF competition and recently awarding about $5 million for improved algorithms (see gocompetition.energy.gov)
- A 2016 National Academies Press report, titled “Analytic Research Founds for the Next-Generation Electric Grid,” recommended improved AC OPF models
  - I would recommend reading this report; it provides good background on power systems include OPF
  - It is available for free at www.nap.edu/catalog/21919/analytic-research-foundations-for-the-next-generation-electric-grid

OPF and SCOPF History

- A nice OPF history from Dec 2012 is provided by the below link, and briefly summarized here
- Prior to digital computers economic dispatch was solved by hand and the power flow with network analyzers
- Digital power flow developed in late 50’s to early 60’s
- First OPF formulations in the 1960’s
  - J. Carpienterm, “Contribution e l’étude do Dispatching Economique,” Bulletin Society Francaise Electriciens, 1962
  - H.W. Dommel, W.F. Tinney, “Optimal power flow solutions,” *IEEE Trans. Power App. and Systems*, Oct. 1968
    - “Only a small extension of the power flow program is required”

www.ferc.gov/industries/electric/indus-act/market-planning/opf-papers/acopf-1-history-formulation-testing.pdf
(by M Cain, R. O’Neill, A. Castillo)

OPF and SCOPF History

- A linear programming (LP) approach was presented by Stott and Hobson in 1978
  - B. Stott, E. Hobson, “Power System Security Control Calculations using Linear Programming,” (Parts 1 and 2) *IEEE Trans. Power App and Syst.*, Sept/Oct 1978
- Optimal Power Flow By Newton’s Method
  - D.I. Sun, B. Ashley, B. Brewer, B.A. Hughes, and W.F. Tinney, "Optimal Power Flow by Newton Approach", *IEEE Trans. Power App and Syst.*, October 1984
- Follow-up LP OPF paper in 1990
  - O. Alsac, J. Bright, M. Prais, B. Stott, “Further Developments in LP-based Optimal Power Flow,” *IEEE Trans. Power Systems*, August 1990

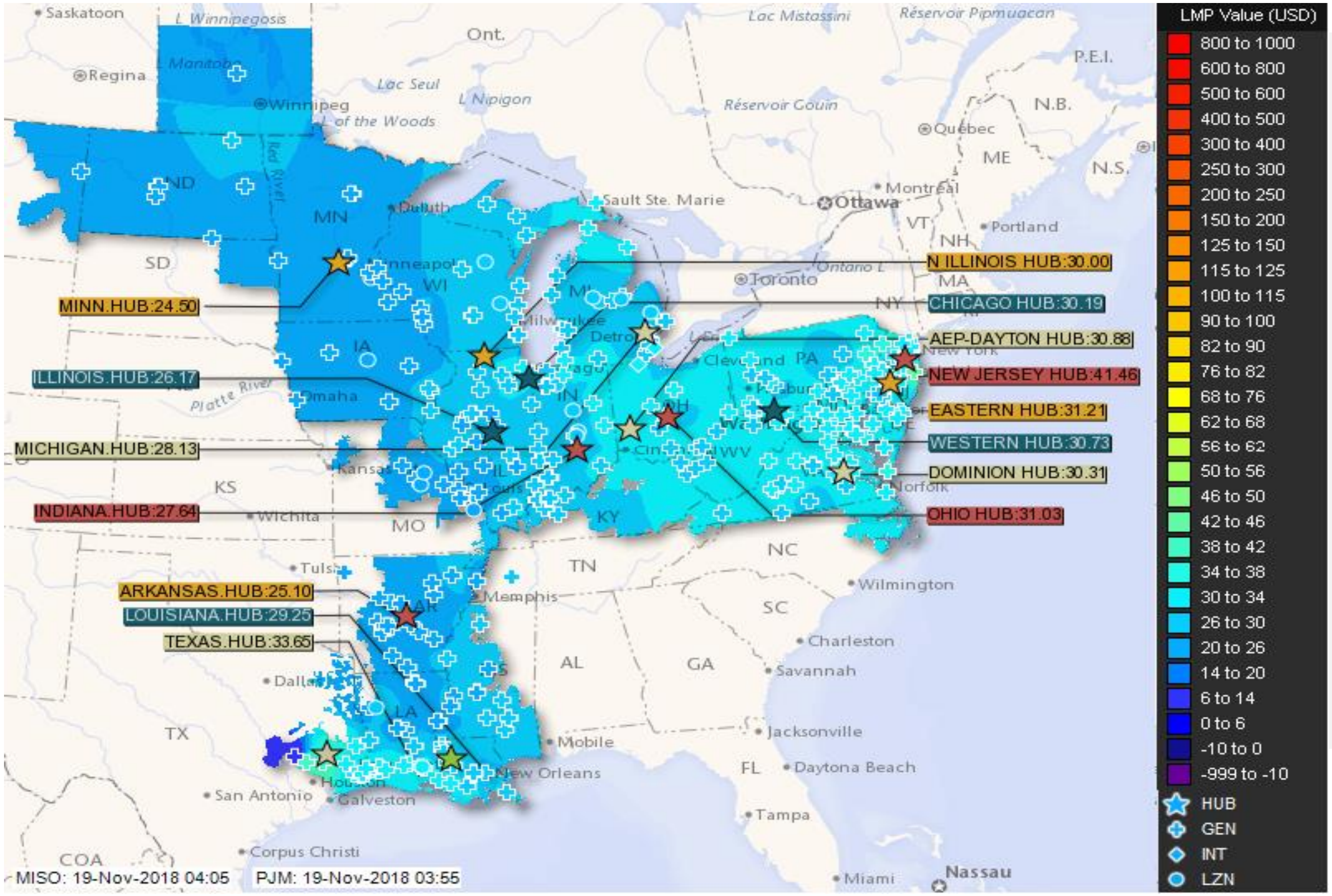
OPF and SCOPF History

- Critique of OPF Algorithms
  - W.F. Tinney, J.M. Bright, K.D. Demaree, B.A. Hughes, “Some Deficiencies in Optimal Power Flow,” *IEEE Trans. Power Systems*, May 1988
- Hundreds of other papers on OPF
- Comparison of ac and dc optimal power flow methods
  - T.J. Overbye, X. Cheng, Y. San, “A Comparison of the AC and DC Power Flow Models for LMP Calculations,” Proc. 37th Hawaii International Conf. on System Sciences, 2004

Key SCOPF Application: Locational Marginal Prices (LMPs)

- The locational marginal price (LMP) tells the cost of providing electricity to a given location (bus) in the system
- Concept introduced by Schweppe in 1985
  - F.C. Schweppe, M. Caramanis, R. Tabors, "Evaluation of Spot Price Based Electricity Rates," *IEEE Trans. Power App and Syst.*, July 1985
- LMPs are a direct result of an SCOPF, and are widely used in many electricity markets worldwide
  -

Example LMP Contour, 11/19/2018



LMPs are now widely visualized using color contours; the first use of LMP color contours was presented in [1]

https://www.miso-pjm.com/markets/contour-map.aspx

[1] T.J. Overbye, R.P. Klump, J.D. Weber, “A Virtual Environment for Interactive Visualization of Power System Economic and Security Information,” IEEE PES 1999 Summer Meeting, Edmonton, AB, Canada, July 1999

OPF Problem Formulation

- The OPF is usually formulated as a minimization with equality and inequality constraints

$$\text{Minimize } F(\mathbf{x},\mathbf{u})$$

$$\mathbf{g}(\mathbf{x},\mathbf{u}) = \mathbf{0}$$

$$\mathbf{h}_{\text{min}} \le \mathbf{h}(\mathbf{x},\mathbf{u}) \le \mathbf{h}_{\text{max}}$$

$$\mathbf{u}_{\text{min}} \le \mathbf{u} \le \mathbf{u}_{\text{max}}$$

where **x** is a vector of dependent variables (such as the bus voltage magnitudes and angles), **u** is a vector of the control variables, F(**x**,**u**) is the scalar objective function, **g** is a set of equality constraints (e.g., the power balance equations) and **h** is a set of inequality constraints (such as line flows)

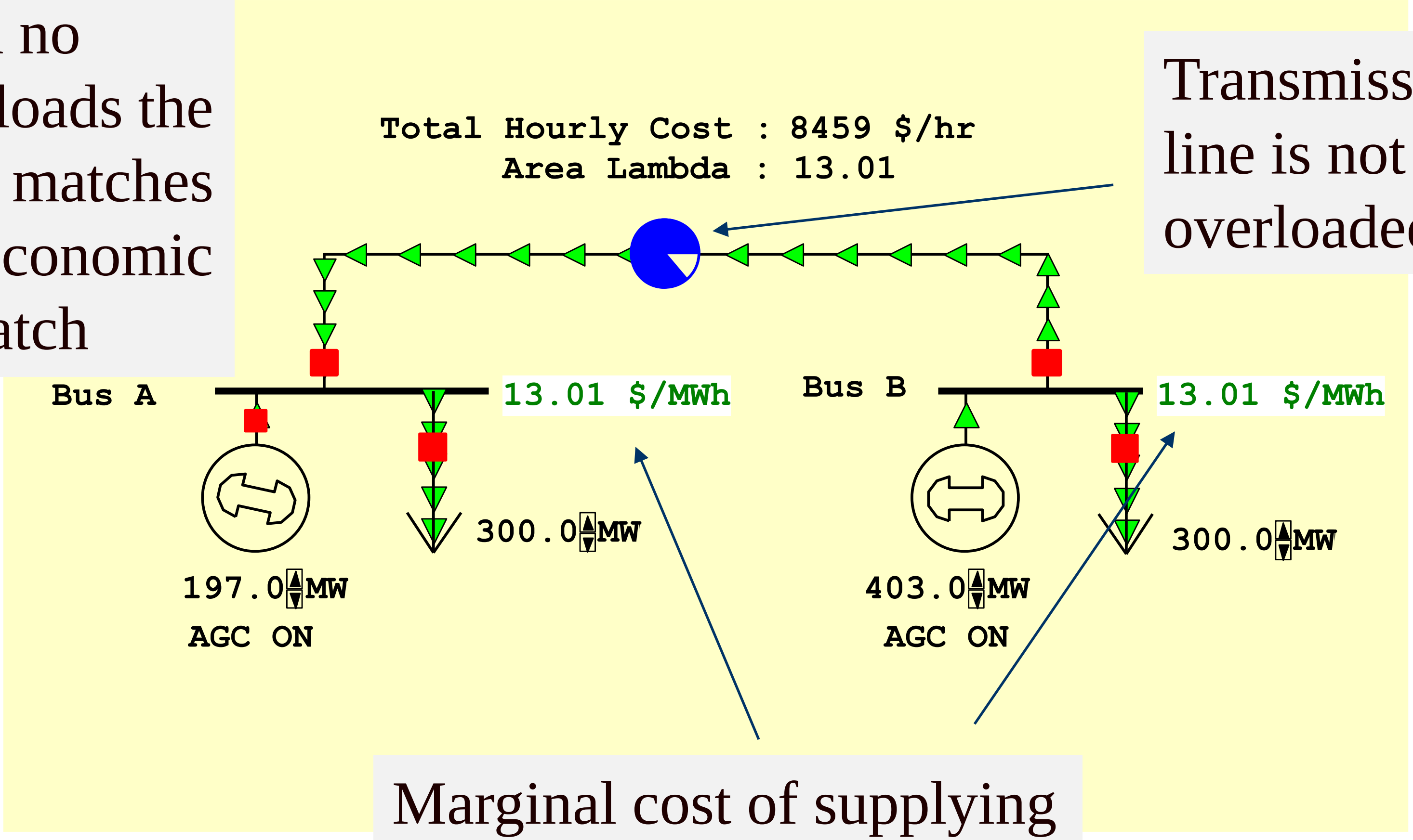
LP OPF Solution Method

- Solution iterates between
  - solving a full ac or dc power flow solution
    - enforces real/reactive power balance at each bus
    - enforces generator reactive limits
    - system controls are assumed fixed
    - takes into account non-linearities
  - solving a primal LP
    - changes system controls to enforce linearized constraints while minimizing cost

Two Bus with Unconstrained Line

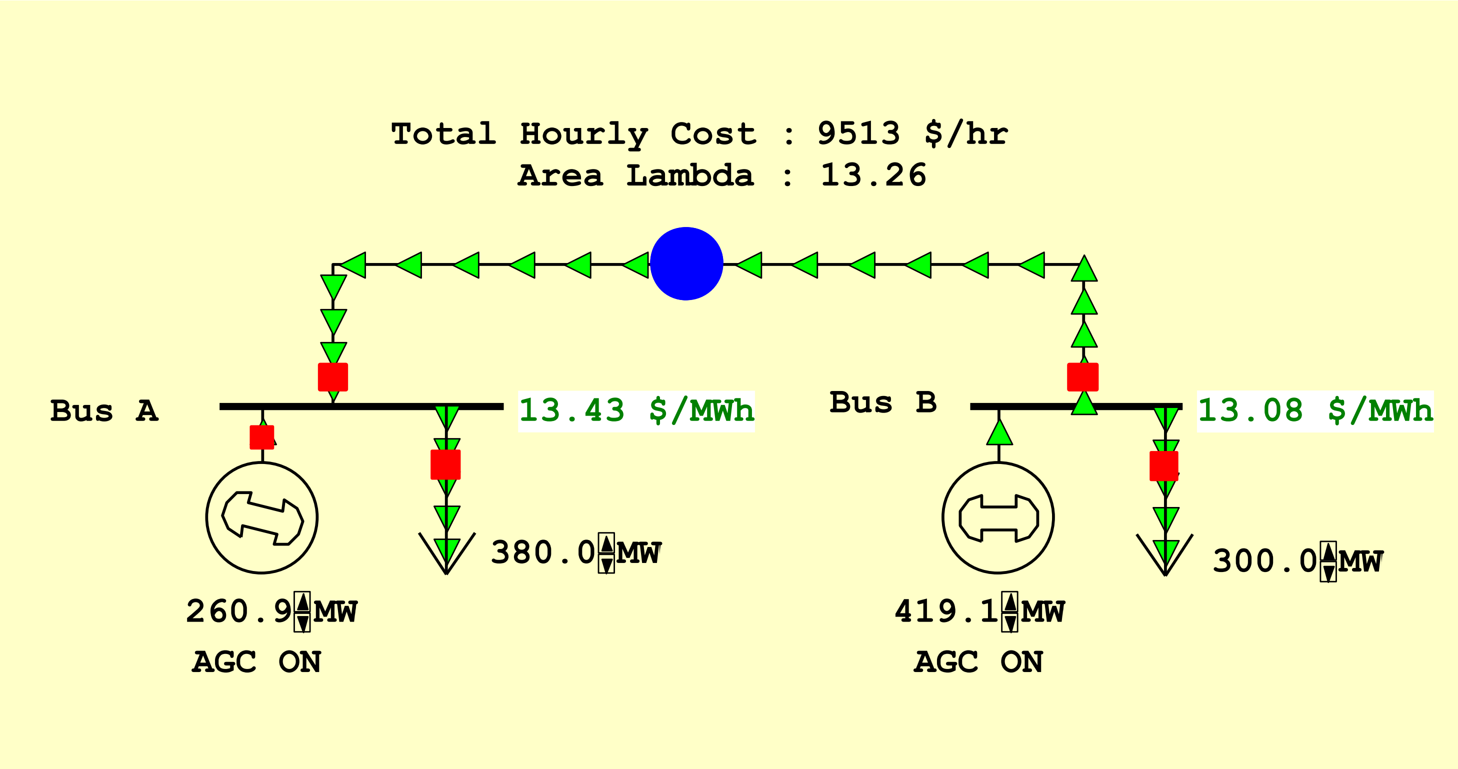
With no overloads the OPF matches the economic dispatch

Transmission line is not overloaded



Marginal cost of supplying power to each bus (locational marginal costs)

Two Bus with Constrained Line

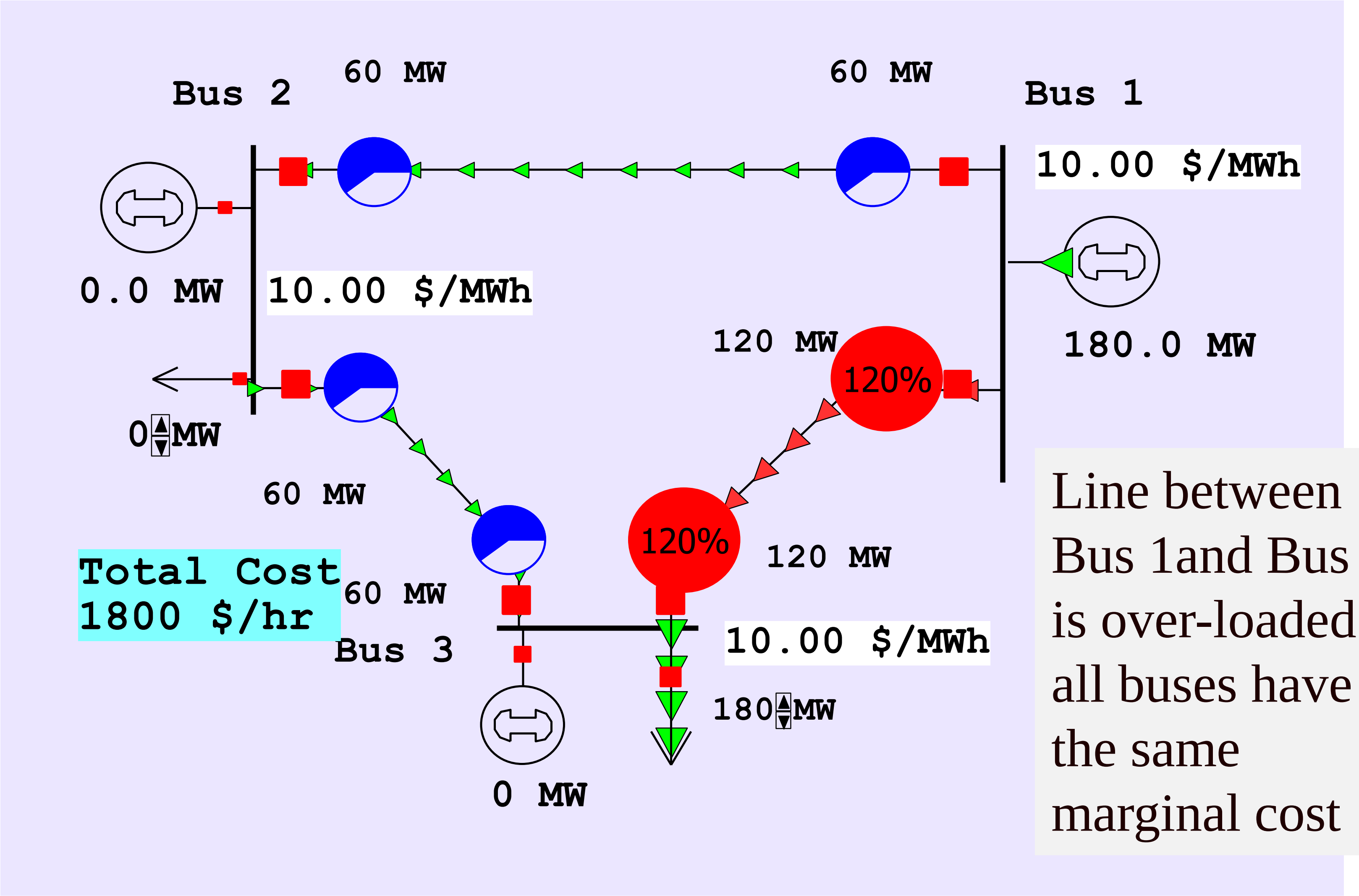


With the line loaded to its limit, additional load at Bus A must be supplied locally, causing the marginal costs to diverge.

Three Bus (B3) Example

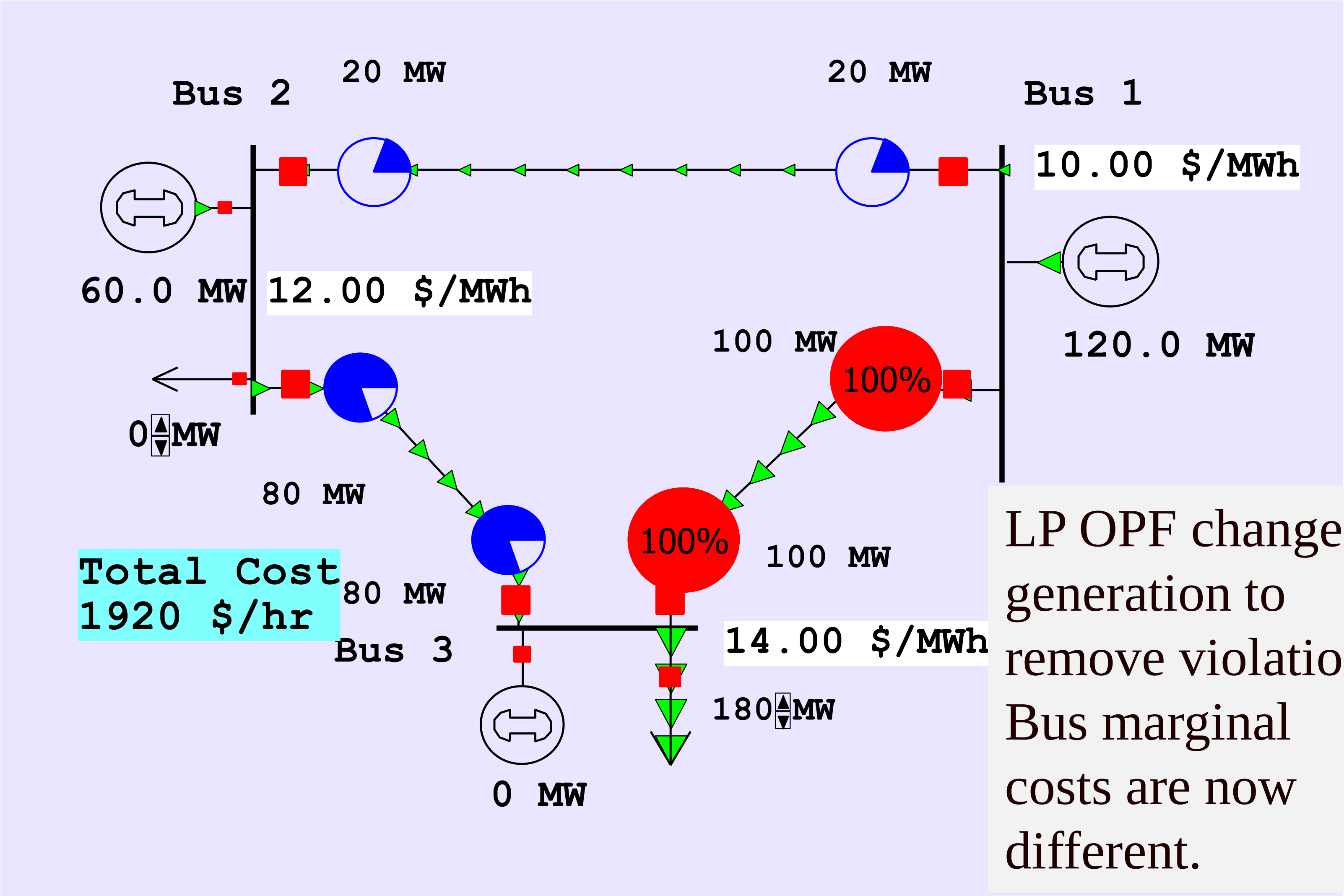
- Consider a three bus case (Bus 1 is system slack), with all buses connected through 0.1 pu reactance lines, each with a 100 MVA limit
- Let the generator marginal costs be
  - Bus 1: 10 $ / MWhr; Range = 0 to 400 MW
  - Bus 2: 12 $ / MWhr; Range = 0 to 400 MW
  - Bus 3: 20 $ / MWhr; Range = 0 to 400 MW
- Assume a single 180 MW load at bus 2

B3 with Line Limits NOT Enforced



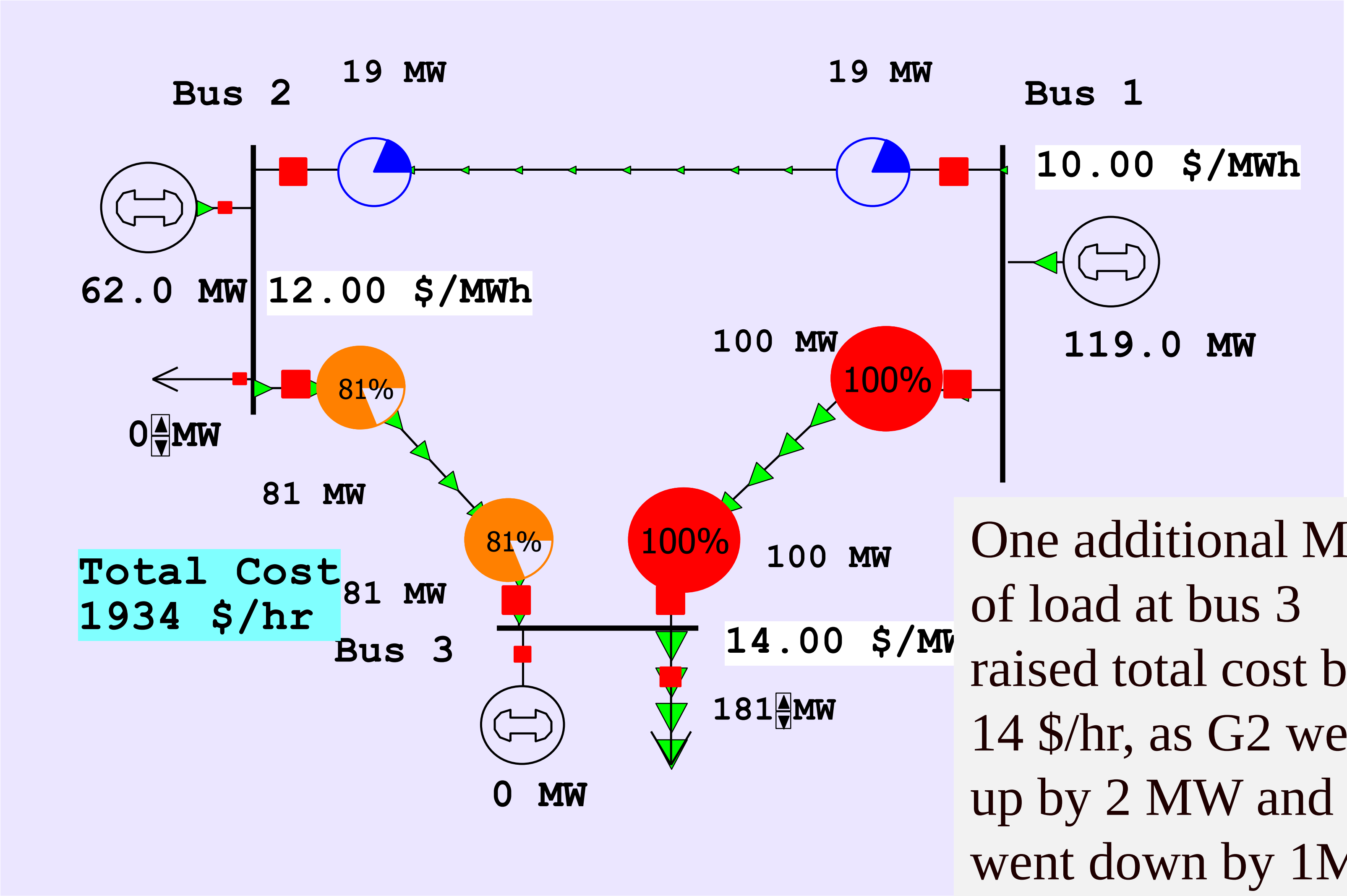
Line between Bus 1and Bus 3 is over-loaded; all buses have the same marginal cost

B3 with Line Limits Enforced



LP OPF changes generation to remove violation. Bus marginal costs are now different.

Verify Bus 3 Marginal Cost



One additional MW of load at bus 3 raised total cost by 14 $/hr, as G2 went up by 2 MW and G1 went down by 1MW

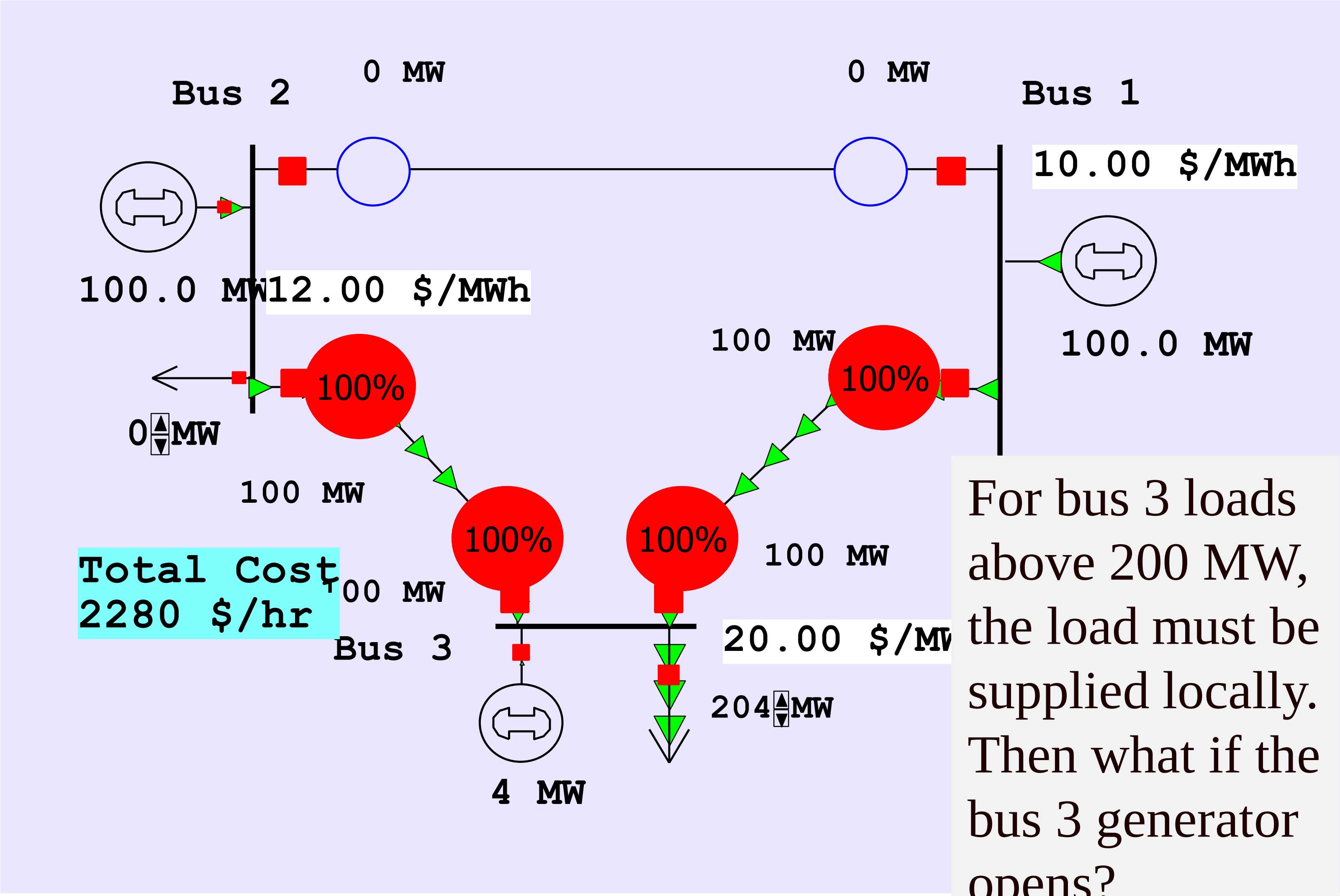
Why is bus 3 LMP = $14 /MWh

- All lines have equal impedance. Power flow in a simple network distributes inversely to impedance of path.
  - For bus 1 to supply 1 MW to bus 3, 2/3 MW would take direct path from 1 to 3, while 1/3 MW would “loop around” from 1 to 2 to 3.
  - Likewise, for bus 2 to supply 1 MW to bus 3, 2/3MW would go from 2 to 3, while 1/3 MW would go from 2 to 1to 3.

Why is bus 3 LMP \$ 14 / MWh, cont’d

- With the line from 1 to 3 limited, no additional power flows are allowed on it.
- To supply 1 more MW to bus 3 we need
  - $\Delta P_{G1} + \Delta P_{G2} = 1$ MW
  - $2/3\ \Delta P_{G1} + 1/3\ \Delta P_{G2} = 0$; (no more flow on 1-3)
- Solving requires we up P_{G2} by 2 MW and drop P_{G1} by 1 MW -- a net increase of \$24 – \$10 = \$14.

Both lines into Bus 3 Congested



For bus 3 loads above 200 MW, the load must be supplied locally. Then what if the bus 3 generator opens?

Quick Coverage of Linear Programming

- LP is probably the most widely used mathematical programming technique
- It is used to solve linear, constrained minimization (or maximization) problems in which the objective function and the constraints can be written as linear functions

Example Problem 1

- Assume that you operate a lumber mill which makes both construction-grade and finish-grade boards from the logs it receives. Suppose it takes 2 hours to rough-saw and 3 hours to plane each 1000 board feet of construction-grade boards. Finish-grade boards take 2 hours to rough-saw and 5 hours to plane for each 1000 board feet. Assume that the saw is available 8 hours per day, while the plane is available 15 hours per day. If the profit per 1000 board feet is $100 for construction-grade and $120 for finish-grade, how many board feet of each should you make per day to maximize your profit?

Problem 1 Setup

Let x_1=amount of cg, x_2= amount of fg

$$\begin{aligned} \text{Maximize} \quad & 100x_1 + 120x_2 \\ \text{s.t.} \quad & 2x_1 + 2x_2 \le 8 \\ & 3x_1 + 5x_2 \le 15 \\ & x_1, x_2 \ge 0 \end{aligned}$$

Notice that all of the equations are linear, but they are inequality, as opposed to equality, constraints; we are seeking to determine the values of x_1 and x_2

Example Problem 2

- A nutritionist is planning a meal with 2 foods: A and B. Each ounce of A costs $ 0.20, and has 2 units of fat, 1 of carbohydrate, and 4 of protein. Each ounce of B costs $0.25, and has 3 units of fat, 3 of carbohydrate, and 3 of protein. Provide the least cost meal which has no more than 20 units of fat, but with at least 12 units of carbohydrates and 24 units of protein.

Problem 2 Setup

Let x_1=ounces of A, x_2= ounces of B

Minimize $0.20x_1 + 0.25x_2$

s.t. $2x_1 + 3x_2 \le 20$

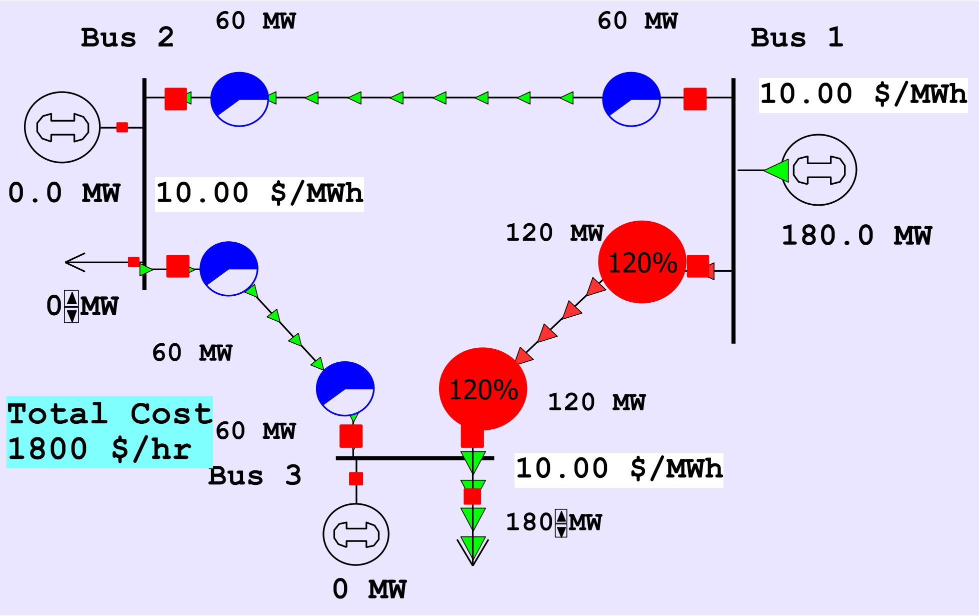
$x_1 + 3x_2 \ge 12$

$4x_1 + 3x_2 \ge 24$

Again all of the equations are linear, but they are inequality, as opposed to equality, constraints; we are again seeking to determine the values of x_1 and x_2; notice there are also more constraints then solution variables

Three Bus Case Formulation

- For the earlier three bus system given the initial condition of an overloaded transmission line, minimize the cost of generation such that the change in generation is zero, and the flow on the line between buses 1 and 3 is not violating its limit



- Can be setup considering the change in generation, (ΔP_{G1}, ΔP_{G2}, ΔP_{G3})

Three Bus Case Problem Setup

Let $x_1 = \Delta P_{G1}$, $x_2 = \Delta P_{G2}$, $x_3 = \Delta P_{G3}$

Minimize $10x_1 + 12x_2 + 20x_3$

s.t. $\frac{2}{3}x_1 + \frac{1}{3}x_2 \le -20$ Line flow constraint

$x_1 + x_2 + x_3 = 0$ Power balance constraint

enforcing limits on x_1, x_2, x_3